

1 **Practical Application of Natural Pozzolans and Lime for**
2 **Cost Optimisation in Low Cost Housing**

3 Dans Nshekanabo Naturinda¹

4 ¹ Makerere University, Kampala, Uganda
5 dnaturinda@cedat.mak.ac.ug

6 **Abstract.** Portland cement is considered one of the costly construction materials.
7 It is sometimes used in applications where its strength levels are not necessary.
8 This study optimized the use of OPC by considering its substitution with
9 pozzolanic materials to reduce construction cost. The pozzolnic material used
10 was volcanic ash which is abundant in many parts of Uganda. The ash was mixed
11 with lime and water. The study examined the pozzolan-lime system to determine
12 its optimum performance for a given pozzolan with known mineral composition.
13 The work was experimental involving testing trial mortar cubes of different
14 pozzolan-lime blends and varying pozzolan particle sizes. The results yielded
15 second order polynomial relationships between the achieved compressive
16 strength and the pozzolan-lime content. The optimum blend was determined from
17 the first derivative of the functions. The blends that would yield the highest
18 possible compressive strength values were derived from the absolute critical
19 points of the polynomials, which when substituted into the functions yielded the
20 actual peak values. Using the best fitting polynomial models, the maximum
21 possible compressive strength values were generated. The blends containing
22 pozzolans of 125microns particle size yielded consistently high peak values for
23 all the experiments. The optimum blend was determined using the 125micron
24 function, and the pozzolan-lime content that yielded consistent results was
25 between 54% and 60%. The achieved compressive strength was 0.9MPa, which
26 is expected to increase for pozzolans with finer particles. The values attained are
27 adequate for a number of low-strength construction applications. The use of OPC
28 can be restricted to only structurally-sensitive elements like beams and columns.
29 This would serve to reduce the demand for OPC in housing construction and also
30 reduce the cost of construction.

31 **Keywords:** Pozzolans, Volcanic Ash, Low-Strength Construction Applications

32 **1 Introduction**

33 Portland cements are the most widely used binders in construction. However,
34 cement-based binders are costly mainly due to high energy requirements for Portland
35 cement production [1]. In spite of its cost, the high demand for Portland cement has
36 been attributed to the little confidence the users have in alternative binders [2]. When
37 used for small buildings and low-strength applications, Portland cement makes

38 construction unnecessarily more expensive than it ought to be. Habitat [3] estimates
39 that up to 80% of the world-wide use of cement does not require strength levels of
40 Portland cement. This can only change if the fitness of purpose of cheaper alternatives
41 is explored to reduce the cost of construction. One such alternative is the use of natural
42 pozzolans with lime.

43 A pozzolan is a material which when finely ground and mixed with lime in the
44 presence of water, reacts to form a cement-like product [4]. Addition of natural
45 pozzolans to lime was found to increase the density and reduce porosity of mortar,
46 which increases its strength and durability [5]. Significant increases in compressive
47 strength of concrete were also registered by various researchers [6] [7].

48 There are vast deposits of natural pozzolans in Uganda especially in form of volcanic
49 soils and other natural earth deposits of similar origin in rift valley areas [8]. Their
50 extensive use in construction has been hindered by the suspect quality of their products
51 and lack of adequate information about their performance.

52 The use of lime binders in construction has become prominent due to its
53 sustainability credentials [9]. Pozzolans have over the years been used to enhance the
54 properties of lime as a binder [10].

55 **2 Objectives, Materials and Methodology**

56 This study was carried out to examine the pozzolan-lime system to determine its
57 optimum performance for a given pozzolan with know mineral composition. The work
58 was experimental involving trial mortar cubes of different pozzolan-lime blends and
59 varying pozzolan particle size, and tested after 7 days, 28 days, and 90 days of curing.

60 A fixed effects model was used with 5 different blending levels selected over a
61 uniform range from 10% to 90%. Each grade of the pozzolan defined by the dominant
62 particle size was divided into five proportionate portions and treated to the lime blends
63 of 10%, 30%, 50%, 70%, and 90%. Each treated portion was mixed thoroughly with a
64 motorised mixer, and the same quantity of water added to each. All the cubes were
65 subjected to the same curing environment, and tested for compressive strength. The
66 procedure used ensured pre-treatment equality of the sample portions by random
67 assignment. The compressive tests were guided by the test procedure prescribed in
68 ASTM311 detailed under Test Method C109/C109M.

69 The experiments focussed on two parameters that were found to have significant
70 influence on engineering performance and cost. These include the pozzolan content
71 (blend) and particle size (grade). The investigation assessed each of the parameters
72 independent of the other, and also considered the likely combined effect on
73 compressive strength development of pozzolans lime mortar. The aim was to establish
74 the nature of the effect of each of these parameters, independently and in combination,
75 on engineering performance in terms of compressive strength development, and the
76 extent and significance of such an effect.

77 3 Results

78 The variations of trends revealed from the assessment of one factor at a time pointed
 79 to the possibility that the observed effect of one factor could actually be dependent on
 80 the level of the other factor at which it occurred. Therefore, examination of the
 81 interaction between the two factors, pozzolan content and particle size, to influence the
 82 observed compressive strength values was conducted. The cross-tabulation of the
 83 findings for 90 days is given in Table 1.

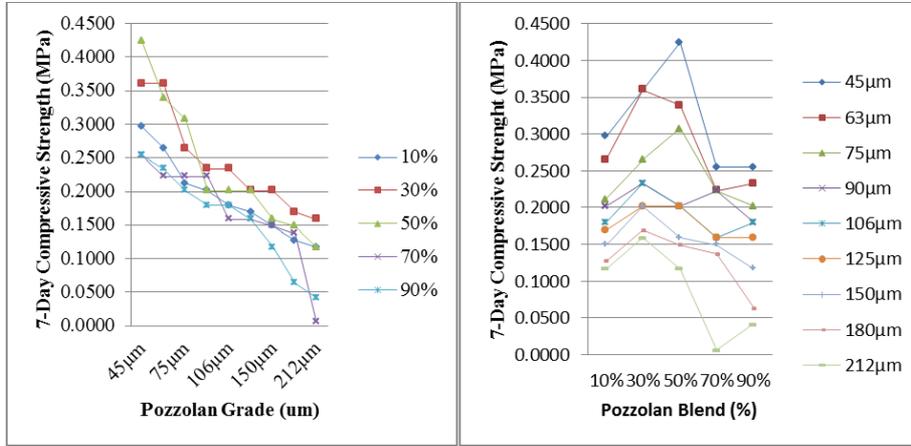
84 **Table 1** Compressive strength variation with pozzolan grade and content

<i>7-Day Tests</i>									
	<i>45μm</i>	<i>63μm</i>	<i>75μm</i>	<i>90μm</i>	<i>106μm</i>	<i>125μm</i>	<i>150μm</i>	<i>180μm</i>	<i>212μm</i>
<i>10%</i>	0.2968	0.2650	0.2120	0.2014	0.1802	0.1696	0.1484	0.1272	0.1166
<i>30%</i>	0.3604	0.3604	0.2650	0.2332	0.2332	0.2014	0.2014	0.1696	0.1590
<i>50%</i>	0.4240	0.3392	0.3074	0.2014	0.2014	0.2014	0.1590	0.1484	0.1166
<i>70%</i>	0.2544	0.2226	0.2226	0.2226	0.1590	0.1590	0.1484	0.1378	0.0064
<i>90%</i>	0.2544	0.2332	0.2014	0.1802	0.1802	0.1590	0.1166	0.0636	0.0424
<i>28-Day Tests</i>									
	<i>45μm</i>	<i>63μm</i>	<i>75μm</i>	<i>90μm</i>	<i>106μm</i>	<i>125μm</i>	<i>150μm</i>	<i>180μm</i>	<i>212μm</i>
<i>10%</i>	0.4134	0.4134	0.3922	0.3604	0.3074	0.2862	0.2650	0.2120	0.0000
<i>30%</i>	0.7950	0.5194	0.4452	0.4240	0.3922	0.3710	0.3710	0.3604	0.2756
<i>50%</i>	0.5512	0.5194	0.4770	0.4452	0.4452	0.3922	0.3074	0.2438	0.2438
<i>70%</i>	0.6360	0.4134	0.4028	0.3286	0.2650	0.2120	0.2120	0.1696	0.1272
<i>90%</i>	0.4558	0.2544	0.2226	0.1272	0.1060	0.0954	0.0636	0.0551	0.0000
<i>90-Day Tests</i>									
	<i>45μm</i>	<i>63μm</i>	<i>75μm</i>	<i>90μm</i>	<i>106μm</i>	<i>125μm</i>	<i>150μm</i>	<i>180μm</i>	<i>212μm</i>
<i>10%</i>	0.5194	0.4664	0.4664	0.4400	0.4240	0.3900	0.3816	0.3500	0.3180
<i>30%</i>	0.8480	0.5830	0.5300	0.5088	0.4770	0.4400	0.4240	0.4000	0.3900
<i>50%</i>	0.6200	0.5600	0.5300	0.5000	0.4982	0.4770	0.4558	0.2120	0.2120
<i>70%</i>	0.6890	0.6800	0.6000	0.5500	0.3710	0.2120	0.1908	0.1590	0.1484
<i>90%</i>	0.3816	0.3816	0.3100	0.2400	0.2120	0.1696	0.1590	0.1378	0.0530

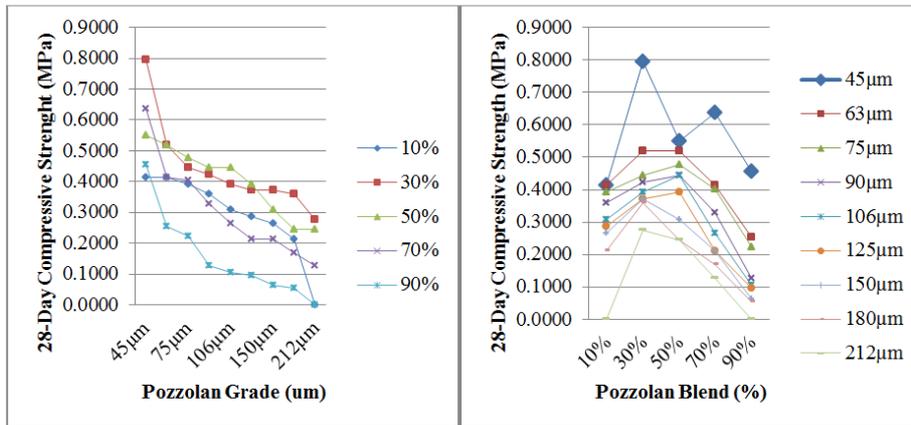
85 This examination established that not only did each factor have an effect on the
 86 observed values, but there was also an influence from interaction between the two
 87 factors. There was no single blend or grade that produced consistently high or low
 88 compressive strength values. As such, the combined effect was found to be more
 89 relevant in determining the behavior of pozzolan-lime mortars.

90 Further examination aimed at optimising the contribution from both. The 50% and
 91 70% blends exhibited the highest interaction between the two factors at 7 days. The
 92 28-day experiments exhibited clear interaction between the two factors for all the
 93 blends except for the 10% and 90% experiments. Observations from long-term
 94 experiments after 90 days showed virtually no interaction for the 10% and 90% blends.
 95 Figure 1 presents the findings for the two-factor interactions.

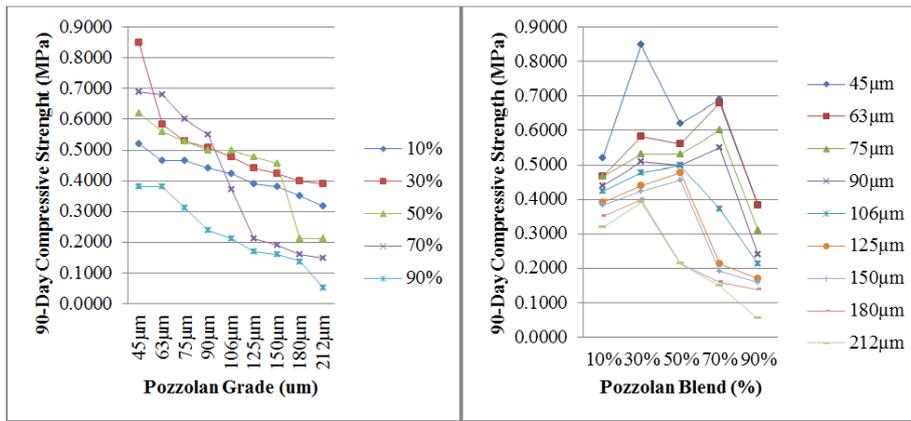
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Figure 1 The two-factor interaction for 7-day, 28-day and 90-day experiments

100 The high interaction exhibited by the 50% and 70% blends at 7 days indicates the need
101 to have both lime and pozzolans in comparable proportions skewed towards more
102 pozzolans. On the other hand, the improved interaction at 28 days can be attributed to
103 prolonged contact between pozzolans and lime that allowed more of the reactive
104 compounds to contribute to the compressive strength development. The 90-day
105 findings affirmed the inference that for higher quantities of either constituent, there is
106 little or no interaction of the dependent variables, and any observations made could be
107 a result of the filler effect of the excess material.

108 **4 Discussion**

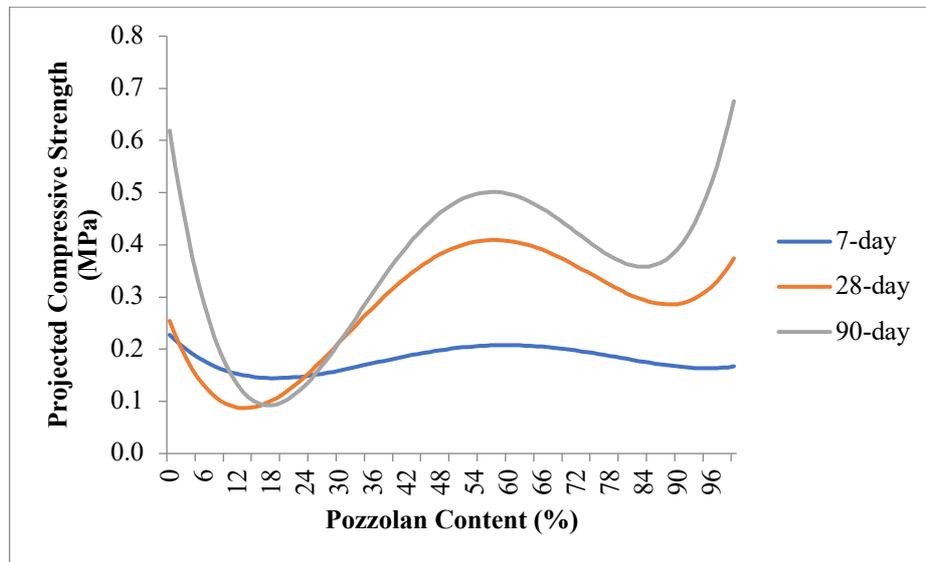
109 The interchange in performance between 50% and 70% mixes with respect to maximum
110 attainable compressive strength and stability against changes in grade over time,
111 implies that in between the two mixes lies the mix that would yield optimum
112 performance. This mix was established by examining the variation of compressive
113 strength with respect to the pozzolan content in the mix. The observations revealed
114 significant interaction of the pozzolan content and pozzolan grade in influencing
115 compressive strength for the 50% and 70% blends. This interaction was consistent for
116 the entire duration of the experiments as opposed to other blends that exhibited
117 interaction only for ultimate strength tests. Interaction was also observed for the fine
118 grades up to 125 μ m. This upper limit of pozzolan grade would enable effective reaction
119 of the pozzolan and lime. Any finer grades would be more expensive to produce, while
120 less fine grades would be less effective in compressive strength development.

121 The experiments generally confirmed that the compressive strength of the pozzolan-
122 lime system increases up to a certain point beyond which it begins to reduce. The peak
123 points for early age compressive strength are skewed to the right. This implies a bigger
124 influence by pozzolans on the early peak compressive strength attainable than lime.
125 However, the peaks are closer to the 50% pozzolan content level than the 90% content,
126 which implies the need for pozzolans and lime in comparable proportions.

127 The pozzolan blends that registered peak early age compressive strength for all
128 pozzolan grades were above 50%. However, these followed no particular trend. This
129 is an indication of no clear link between the blend that gives peak strength and the
130 pozzolan grade. While the compressive strength generally increases with finer grades,
131 it was not the case with the critical blends producing peak compressive strength values.
132 This suggests greater stability for pozzolan content with respect to compressive strength
133 variability. Hence, irrespective of the pozzolan grade, the range of the pozzolan content
134 that gives peak strength varied less.

135 Where two factors are contributing to the observed effect, the effect of each factor
136 depends on which level of the other factor it occurs [11]. This is a result of the
137 interaction of the two factors in contributing to the observed effect. It was therefore
138 important to establish the level or range of each of the factors within which the observed
139 effect is optimised sustainably and consistently. The derived polynomial expressions
140 were used to predict the range within which interaction consistence is maintained. The
141 pozzolan content was varied between 0% and 100% in the 7-day, 28-day, and 90-day

142 experiments with the 125 μ m grade to obtain the resultant illustrations given in Figure
 143 2.



144

145 **Figure 2** Prediction of optimal strength development in the pozzolan - lime system

146 It can be observed that the range of pozzolan content that gives the same strength values
 147 for the same duration irrespective of the pozzolan content is 47% to 68%. It is in this
 148 region that there is noticeable increase in compressive strength values between 7-day,
 149 28-day, and 90-day experiments, irrespective of the pozzolan content. The best results
 150 are however obtained in the range of 54% to 60% pozzolan content.

151 5 Conclusions

152 It can be deduced from the findings that the best compressive strength performance
 153 values can be obtained in the pozzolan-lime system if the predominant pozzolan particle
 154 size is in the range of 125 μ m, and the pozzolan content between 54% and 60%.

155 The maximum strength attainable for any grade is less sensitive to pozzolan
 156 content, provided adequate pozzolans are available to react with the available lime.
 157 This is important in practice as it may not be practical to have strict content guidelines
 158 for a craftsman using the material. This should provide confidence in application
 159 because the less sensitivity of attainable strength values over a wide range of pozzolan
 160 content values allows for greater flexibility when using the material.

161 The registered peak value for compressive strength was 0.9MPa. This is much more
 162 inferior to that attained with Portland cement, but would pass for a number of low-grade
 163 mortars and low-strength construction applications like mortars and soil stabilization.

164 **References**

- 165 1. Day R. L. (1990), Pozzolans for use in low-cost housing. A report for the International
166 Development Research Centre, Ottawa.
- 167 2. Spence R. C. S. (1980), Small scale production of cementitious materials. Intermediate
168 Technology Publications, London, United Kingdom.
- 169 3. Habitat (1985), The use of selected indigenous building materials with potential for wide
170 application in developing countries. United Nations Centre for Human Settlements, Nairobi.
- 171 4. Kerali A.G., Mwakali, J.A., and Okure, M.E. (2007), Development and application of
172 construction materials in Uganda. Fountain Publishers, Kampala.
- 173 5. Malisa A. S., Park E., and Lee J. (2014), Effect of Lime on Physical Properties of Natural
174 Pozzolana from Same, Tanzania. International Journal of Engineering Research and
175 Technology, Vol. 3, Issue 11, November 2014.
- 176 6. Osei D. Y. and Jackson E. N. (2012), Compressive Strength and Workability of Concrete
177 using Natural Pozzolana as Partial Replacement of Ordinary Portland Cement. Advances in
178 Applied Science Research; Pelagia Research Library, Coden USA.
- 179 7. Rahmaa A. and Jomaa H. (2018), Modeling the Cementitious Effect of the Pozzolana on
180 the Compressive Strength of Concrete. Cogent Engineering (ISSN: 2331-1916), 5:1548002.
- 181 8. Department of Geological Surveys and Mines (1992), Pozzolan housing project. A report
182 for the International Development Research Centre, Ottawa.
- 183 9. Warker R. and Pavira S. (2010), Behaviour and Properties of Lime-Pozzolan Pastes.
184 Proceedings of the 8th International Masonry Conference, Technische Universitat Dresden.
- 185 10. Massaza F. (2002), Properties and Applications of Natural Pozzolans, Structure and
186 Performance of Cements. Bensted J. and Barnes P. (Eds), Spon Press, London
- 187 11. Navidi W., (2008), Statistics for engineers and scientists. 2nd Edition, McGraw-Hill
188 International Edition, New York.